WATER RETICULATION AND DRAINAGE IN BUILDINGS

SANS10252-1 SANS10400-W SANS10252-2 SANS10400-P

WATER RETICULATION IN BUILDINGS

LEGISLATIVE BACKGROUND



Government Notice R509 of 08 June 2001

Water Services Act (Act 108 of 1998)

- 13(2) If constructed or installed after promulgation of these Regulations, a suitable water volume measuring device or volume controlling device must be fitted to separately measure or control the water supply to every –
 - (a) individual dwelling within a new sectional title development, group housing development or apartment building;
 - (b) individual building, having a maximum designed flow rate exceeding 60 litres per minute within any commercial or institutional complex;

14. Every consumer installation <u>must</u> comply with SANS 10252: Water Supply (Part 1) and Drainage for Buildings (Part 2) and SANS 10254: The Installation of Fixed Electric Storage Water Heating Systems, or any similar substituting re-enactment or amendment thereof if the consumer installation is of a type regulated by either standard.



National Building Regulations

National Building Regulations and Standards Act
(Act 103 of 1977)

A2 Plans and Particulars to be Furnished

- (1) Any person intending to erect any building, <u>shall</u> submit to the local authority the following plans and particulars, together with the application:
 - (v) particulars required in terms of <u>any applicable</u> <u>legislation</u>, by-laws, or part of SANS 10400;

A7 LAYOUT DRAWING

Any layout drawing contemplated in regulation A2(1)(b) shall indicate the occupancy classification, and shall consist of as many plans, sections, elevations and such other details as may be necessary to show.

(m) where provided, the location, type and capacity of water heating installations;

A8 PLUMBING INSTALLATION DRAWINGS AND PARTICULARS

(1)(a) The provisions of regulation A2(1)(c) [a fire installation drawing] and A2(1)(d) [drainage installation drawing] shall not be construed as preventing the details contemplated in subregulations (2), (3), (4) and (5) being clearly indicated on any layout drawing required in terms of regulation A2(1)(b).

- (2) Any drawing of a fire installation as contemplated in regulation A2(1)(c) shall contain as many plans, sections and elevations as may be necessary to show, where relevant, the following:
 - (a) The location and size of any existing or proposed communication pipe serving or intended to serve any building or site;
 - (b) the location of any pipe, the size of such pipe and the material of which it is manufactured;
 - (c) the location and capacity of any storage tank;
 - (d) the location of any overflow;
 - (e) the location of any pump; and
 - (f) the pressure for which the installation has been designed.

XA ENERGY USAGE IN BUILDINGS

XA2 At least 50% (volume fraction) of the annual average hot water heating requirement shall be provided by means other than electrical resistance heating including but not limited to solar heating, heat pumps, heat recovery from other systems or processes and renewable combustible fuel.

WATER RETICULATION IN BUILDINGS

HOW TO COMPLY (RESIDENTIAL UNITS)

WHAT IS IMPORTANT?

- Water supply
- Water pressure
- Water quality

NOTE:

None of the above can be guaranteed by a water service authority due to several reasons, therefore we may require

- Emergency storage
- Boosting of pressure

WATER QUALITY

7.1.2 Water supply quality — Human consumption

Conditions unfavourable for the development of the bacterium Legionaella pneumophila shall be maintained as far as possible in installations where cold water is stored for drinking purposes, or where hot water could be used for drinking purposes. For this reason,

- a) the presence of organic matter in the water as well as the final products of metal corrosion, mainly iron, shall be kept to a minimum,
- b) compositions of rubber used shall not form a source of nutrient for the bacterium,

- c) storage tanks shall be regularly cleaned and kept free of contamination,
- d) stored cold water shall be maintained at a temperature not exceeding 20 °C,
- e) in a hot water installation, there shall be no zones where water is stored at temperatures of between 25 °C and 45 °C,
- f) the stored hot water shall be maintained at a temperature of at least 55 °C, and
- g) the quality of the water shall be such as to comply with SANS 241-1 and SANS 241-2.

WATER DEMAND

Demand, or volume of water needed per period, is related to the number of people in the building who will be using the water.

NBR A21: Design population

SANS10252-1: Table 1

Table 2

Table 3

NBR A21

(1) The population of any room or storey or portion thereof shall be taken as the actual population of such room, storey or portion thereof where such population is known or, where such population is not known, the population shall be calculated from the criteria given in table 2.

1	2 Population		
Class of occupancy of room or storey or portion thereof			
A1, A2, A4, A5	Number of fixed seats or 1 person per m2 if there are no fixed seats.		
E1, E3, H1, H3, H4	2 persons per bedroom		
E4	16 persons provided that the total number of persons per room is not more than 4		
H5	16 persons per dwelling unit provided that the total number of persons per room is not more than 4		
Ğ1	1 person per 15 m ²		
J1, J2, J3, J4	1 person per 50 m ²		
C1, E2, F1, F2	1 person per 10 m ²		
B1, B2, B3, D1, D2, D3	1 person per 15 m ²		
C2, F3	1 person per 20 m ²		
A3, H2	1 person per 5 m ²		

SANS10252-1

4.2.1.2 An estimate shall be made

- a) of the total daily water demand, using table 1 and table 2, or using any other approved data,
- b) of the probable (or design) flow demand, in accordance with 4.2.2, and
- of the total hot water demand, in accordance with 4.2.3, and of the time of peak hot water demand in terms of 4.2.3.2.

Table 1 — Daily water demand for different premises (excluding garden use)

1	2
Premises	Water demand (including hot water)
Boarding schools ^a , children's homes and residential nurseries	135 L to 200 L per capita
Educational institutions	40 L to 50 L per capita
Kitchens (full meal preparation)	8 L to 12 L per meal prepared
Multiple dwelling units, such as flats	300 L to 400 L per dwelling
Hotels, boarding houses, motels and nurses' homes: with resident staff without resident staff	200 L to 300 L per bed 200 L to 250 L per bed
Commercial premises:	
shops (staff only)	14 L to 18 L per 10 m ² gross floor area
superstores, such as hypermarkets and warehouses	125 L per WC pan, or per 600 mm width of slab urinal
offices with canteens	10 L to 15 L per 10 m² gross floor area
offices without canteens	7 L to 10 L per 10 m² gross floor area
Clinics, hospitals, nursing homes and old-age homes	450 L to 550 L per bed
Factory ablutions	100 L to 200 L per capita
* Excluding kitchen but including laundry.	

Table 2 — Average water consumption (hot and cold) of appliances

L/operation 80 - 90 6 - 8 60 - 180 3 - 70 10 - 15 ⁴ 3 - 6 ⁸ 4 - 8 8 - 10
6 - 8 60 - 180 3 - 70 10 - 15 ⁴ 3 - 6 ⁴ 4 - 8
L/day/person served
3 - 6 18 - 22 10 - 15 20 - 30 8 - 12 32 - 40
L/day/person served
8 - 15 3 - 7 10 - 18 4 - 6 12 - 18 4 - 6

4.2.3 Hot water demand

- 4.2.3.1 For the assessment of the hot water demand, the following factors shall be considered:
- a) the influence that the type of activity performed in the building might have on the demand pattern;

And

 b) the influence that external environmental factors (for example, climate) might have on the demand pattern.

Differentiation between the peak and the design hot water demand is advised so that the implications of an installation not meeting the peak demand can be recognized.

Table 5 — Hot water demand, storage and heater plower requirements.

	2	3	- 4
Premises	Total hot water demand	Storage volume	reaser power"
Chreco	[120 to 150] Libida/II	(30 to 35) Little5id	T.S.KWDolla
Enleges and schools Day school Boarding school*	(16 to 12) L/capital/d (50 to 115) L/capital/d	48 to 6) L/capita (25 to 50) L/capita	0.1 kW Quita (0.5 to 0.20 Arkicapita
Dwelling houses." Low rental Medium to high rental	(80 to 115) L/capita/d (115 to 140) L/capita/d	(100 to 150) (Amit (40 to 50) (Acapta	C2 SWant
Factorial Staff Abstore	(10 to 20) L/capitaid ¿30 to 60) L/capitaid	(5 to 7) L/capita/d (30 to 600 L/capita/d	WisWicapita U 20 Wincapita
Flats (blocks) Low rengal Medium to high rental	(50 to 70) L/ceptard (516 to 140) L/ceptard	(26 to 25) L/capital (25 to 35) L/capital	State to the knowledge
Heightols.	Security of the second	Townson and town	5
Constit InterSouls InterSouls Information Information Information Internal Internal Internal Internal	(130 to 140) L/budde (220 to 230) L/beddi (65 to 79) L/beddi (65 to 95) L/capitald (220 to 230) L/beddi (65 to 95) L/capitald (630 to 130) L/capitald	(25 to 35) Libered (40 to 55) Libered (40 to 55) Libered (40 to 55) Libered (40 to 25) Libered (40 to 25) Libered (40 to 55) Li	
Hostets	(60 to 120) L/capita/d	(30 to 355 L/c 0 to/d	60.8 to 1.15 kW/capitor
Hotels with resident staff withing tradent staff	(120 to 1405 L/bedid (100 to 130) L/bedid	(50 to 70) Grand (60 to 60) Grand	(0.5 to 1.2) Wilted (0.6 to 1,1) Wilted
Krichens Full meal preparation	6/10/75 Limest	(5 to out med	D.I Ny/meat
Offices: with conference without conference	(25 to 26) L/supita/d (10 to 12) L/capita/d	(20 Kitay) L/capita/d (6 jp. 3 L/capita/d	0.5 AW/capta 0.1 AW/capta
Shops istaff only	190 to 12) Dooplast	6) Usapta	0.1 kW/capita
Sports paydions sparcepants only)	(30 to 40) L/capitord	(30 to 40) L/GapRa/d	(1,5 to 2) (W/capita

Refere to direct electrical heating elements only.
Cacheding the kitchen but including the laundry.
Storage normally a minimum of 115 L with a 4 ft heat-up period.

EXAMPLE

Domestic residence (H4), 3 bedrooms

Hot water demand:

NBR A21: 2 persons per bedroom

 $3 \times 2 = 6$ persons

SANS10252-1 Table 5:

6 × 140l/person = 840l

This will be the demand over a 24h period.

Storage required depends on heating cycle of the heater.

DIFFERENT TYPE OF WATER HEATERS & ASSOCIATED STORAGE

- Conventional electrical element
 - Approx. 50l/capita (4h/140l)
- Solar without backup electrical element
 - 120% of daily demand under winter conditions
- 3. Solar with backup electrical element
 - 100% of daily demand under summer conditions
- 4. Solar with backup electrical element
 - total hot water demand
- Instantaneous
 - No storage

Calculate the storage capacity required to achieve maximum efficiency for a 2 bedroom dwelling for

- Conventional electric element geyser
- Solar geyser without backup element
- Solar geyser with backup element

Calculate the storage capacity required to achieve maximum efficiency for a 2 bedroom dwelling for

Conventional electric element geyser

$$2 \times 2 = 4$$
 persons

$$4 \times 50\ell = 200\ell$$

Calculate the storage capacity required to achieve maximum efficiency for a 2 bedroom dwelling for

Solar geyser without backup element

$$2 \times 2 = 4$$
 people

$$4 \times 140\ell = 560\ell$$

Calculate the storage capacity required to achieve maximum efficiency for a 2 bedroom dwelling for

Solar geyser with backup element

$$2 \times 2 = 4$$
 people

$$4 \times 140\ell = 560\ell$$

NATIONAL BUILDING REGULATIONS

XA2 At least 50% (volume fraction) of the annual average hot water heating requirement shall be provided by means other than electrical resistance heating including but not limited to solar heating, heat pumps, heat recovery from other systems or processes and renewable combustible fuel.

- Conventional electrical geyser not compliant
- Solar geysers and heat pumps with backup elements will only be compliant if correctly installed with correct minimum storage capacity

$$Q = \frac{hot \ water \ per \ person \times 365 \ days}{50\%}$$

A20 Classification: H4

A21 Occupancy: 2 persons/bedroom

Type of hot water generation: Solar with back-up element

Hot water demand (SANS10252-1): 140ℓ per day per person

Number of Bedrooms: 3

Total demand: 3 × 2 × 140 = 840€

Hot water storage capacity required: 840 × 50% = 420ℓ (50% XA2)

Capacity provided: 3000 + 1500

A20 Classification: H1

A21 Occupancy: 2 persons/bedroom

Type of hot water generation: Solar with back-up element

Hot water demand (SANS10252-1): 140€ per day per bed

Number of Bedrooms: 10

Total demand: 10 × 2 × 140 = 2800€

Hot water storage capacity required: 2800 × 50% = 1400ℓ (50% XA2)

Capacity provided: 5 × 300%

GUIDELINE: STORAGE CAPACITY OF DOMESTIC SOLAR GEYSERS WITH BACKUP ELEMENT

	EFFICIENT	XA2
1 Bedroom	2301 - 2801	1158 - 1408
2 Bedroom	4601 - 5601	2301 - 2801
3 Bedroom	690l - 840l	3451 - 4201
4 Bedroom	9201 - 1 0401	4601 - 5601

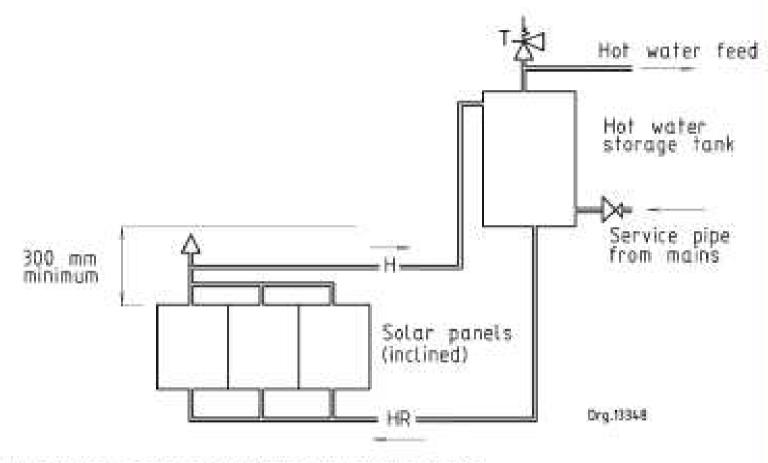
SANS1307 - Domestic storage solar water heating systems

4.5.5 Frame and stand

- 4.5.5.1 Any stand or frame that carries a storage tank on top of a roof shall comply with the following:
- a) The stand shall include a structurally sound load spreading support that evenly distributes the loads, on the rear legs and that protrudes at least 300 mm past each leg.
- b) The stand shall include cross braces that stabilize the frame.

- 4.5.5.2 Any stand or frame that will determine the angle of the collectors or the storage tank (or both) shall comply with the following:
- a) The stand or frame shall allow for the system to be installed at the inclination specified by the manufacturer, on any roof pitch as nominated by the manufacturer.
- b) The manufacturer shall provide clear instructions on how to adjust the inclination of the frame.
- After adjustment the frame shall still comply with all material, corrosion and structural requirements stated in this standard.

SANS10160 - The installation, maintenance, repair and replacement of domestic solar water heating systems



NOTE His the hot water pipe and HR is the hot water reverse pipe.

Figure 2 — Thermosiphonic hot water system

Design considerations and positioning of solar collectors

Solar heaters effectively absorb heat from the sun from about 10:00 until about 16:00.

Solar irradiance is at its peak between about 12:00 and 14:00.

However, sufficient quantities of hot water have to be stored for use after 16:00.

A critical factor in the installation of solar heating systems is the position of the collector relative to the movement of the sun. In the southern hemisphere, collectors should be pointed true north and tilted at an angle above the horizontal equal to the latitude of the site plus 10°.

This angle is chosen mainly to favour the collection of solar heat during winter when the sun is fairly low in the sky, to obtain year round efficiency.

A deviation of up to 45° east or west of north may, however, be acceptable in many cases.

The design of the absorber unit can vary from a simple flat plate to an evacuated tube reflector type absorber.

Ideally, the exposed surface of the collector should absorb the maximum amount of incident solar radiation with a minimum of heat loss. The transparent cover over the collector prevents ingress of rain, reduces the cooling effect of outside air movement over the collector and restricts re-radiation losses, the latter probably being the most important.

This means that the incident solar radiation has to be transmitted through the transparent cover with a minimum loss of heat energy due to absorption.

Thermosiphonic circulation can be created by placing the absorber at the lowest point of the system.

The resulting circulation pressure is fairly small and any obstruction or an accumulation of air bubbles in the system can impede the natural flow of the water.

The absorber and all pipes are therefore sloped in such a way that air can escape to the tank to be vented off.

While the thermosiphonic system is the most popular one for domestic applications, pumped systems permit greater freedom in the placement of the absorber(s), which can then be situated either above or below the storage tank.

A typical pumped system is shown in figure 3. Pumped systems can be direct (where the potable water itself circulates through the solar collector) or indirect as shown in figure 4, where the potable water is heated via a heat exchanger.

In an indirect system, additives can be added to the solar panel water (or primary circulating water) to control corrosion.

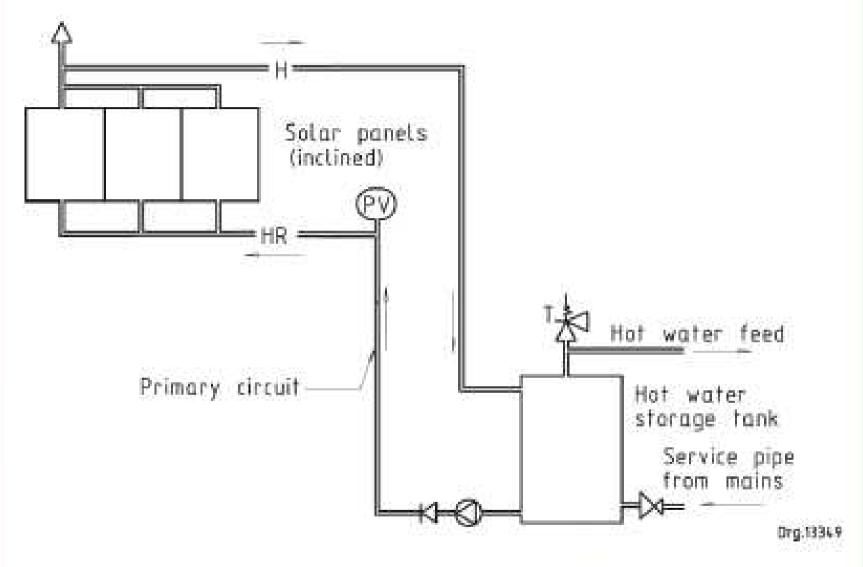


Figure 3 — Pumped direct solar hot water system

Figure 5 shows a more complex arrangement in which a solar installation is used to preheat the feed tester for the main hot water storage tank.

Indirect systems are less efficient than direct systems, owing to losses from the heat exchanger.

Indirect systems do, however, have the following advantages over both thermosiphonic and pumped direct systems:

- a) frost damage can be prevented by the use of a suitable heat transfer fluid, usually water with an antifreeze additive;
- b) damage due to boiling can be prevented if a suitable heat transfer fluid with a high boiling temperature is selected;

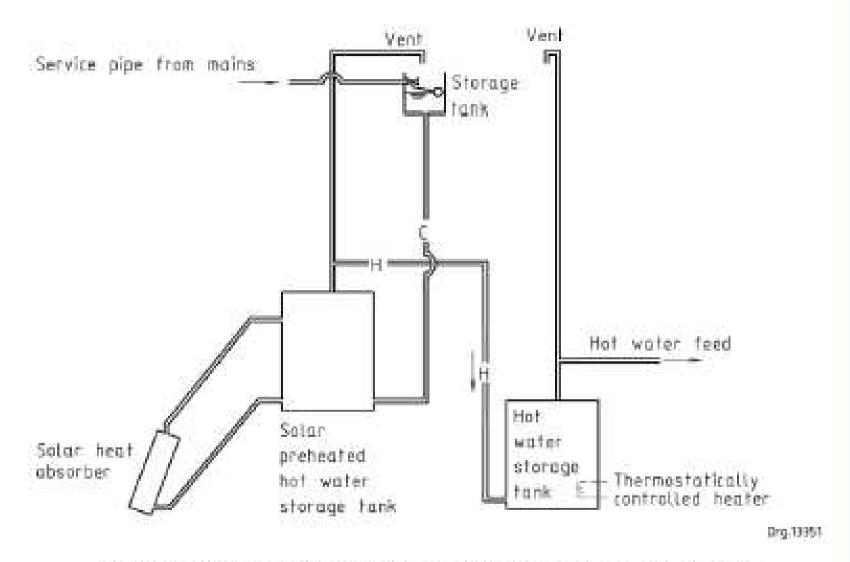


Figure 5 — Solar water heater used for preheating in a hot water system

- c) corrosion within the primary system can be minimized by the use of a corrosion-inhibited heat transfer fluid; and
- d) scale formation within the primary system can be more effectively controlled.

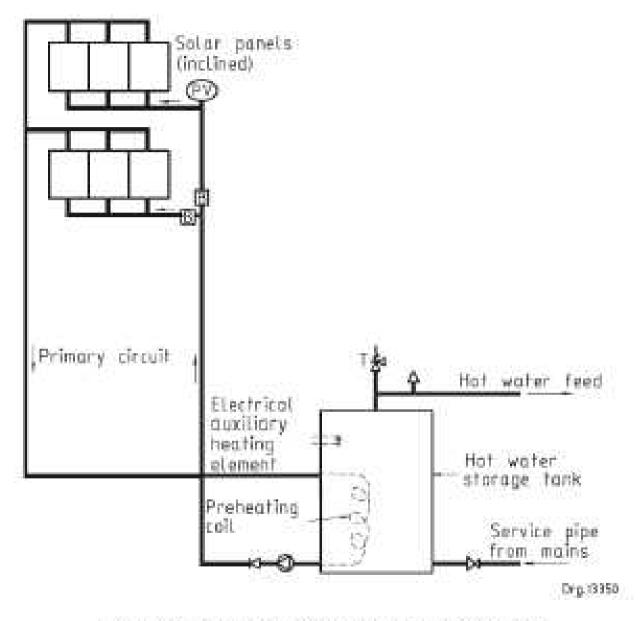


Figure 4 — Pumped indirect solar water system

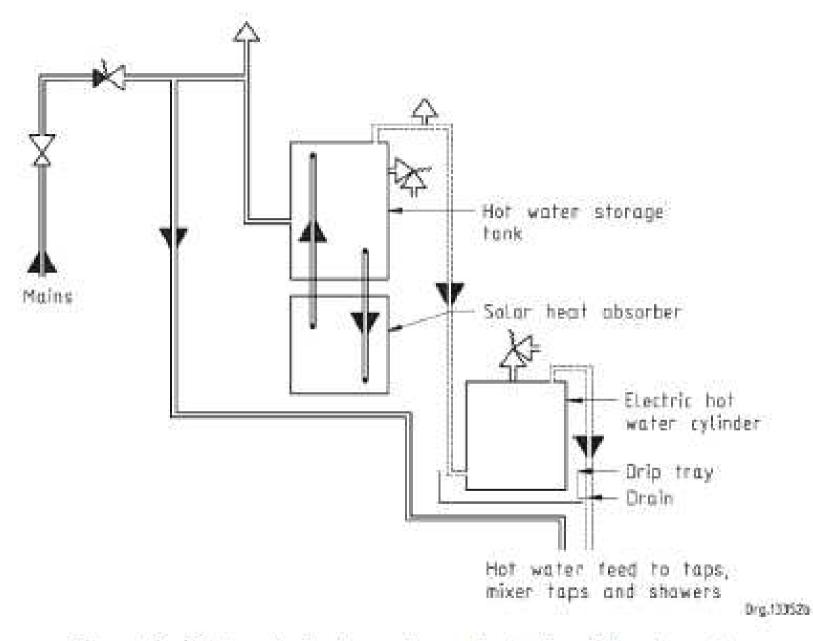


Figure 6 — Solar water heater used as preheater in a hot water system

SANS1352 - The installation, maintenance, replacement and repair of domestic air source water heating heat pump systems

4.3.5 Locating and positioning of the heat pump unit and components

Notwithstanding any National standard the heat pump unit and components shall be located and installed in accordance with the manufacturer's instructions and in such a manner and position to ensure:

- a) the safe and effective operation (both mechanical and electrical) of the system and of each individual component part;
- b) the safe, easy, effective and correct removal and replacement of component parts or spare parts during maintenance, replacement or repair,

- c) the effective discharge and drainage of condensation water from the heat pump unit;
- d) the provision of adequate and sufficient ventilation and airflow stream around the heat pump unit, so as not to impede energy efficiencies or the performance of the heat pump unit (or both);
- e) the prevention of the build up of water, snow, ice, dirt and debris;
- f) the minimisation of noise transmission of the heat pump unit into the environment especially during the night. The noise transmission of the heat pump unit shall not be greater than 45 decibels between 11:00pm and 7:00am and 55 decibels at other times;
- g) that, and not withstanding 5.5.1(a) and 5.5.1(b), the pipe network layout for the heat pump units primary circulation loop shall be such that length and directional changes are minimized;

- h) that the heat pump unit can be supplied with electrical power in an effective and safe manner;
- i) that the orientation of the heat pump unit should be such that the heat pump unit is exposed to the maximum incident solar radiation;

In the southern hemisphere, to ensure maximum operating efficiency, the heat pump unit should preferably be positioned on the northern side of the dwelling. If this is not possible the heat pump unit should be mounted in order of preference, to (1) either north east or north west side, (2) then on east or west side of the dwelling and then only south east or south west and finally on the (3) South face side of the dwelling.

- j) that adverse weather conditions such as high winds and heavy rains or excessive water discharges onto the heat pump unit do not affect the efficient and effective operations of the heat pump unit;
- k) when the heat pump unit is positioned above the storage water heater, provision shall be made to prevent the heat pump unit from draining of water.

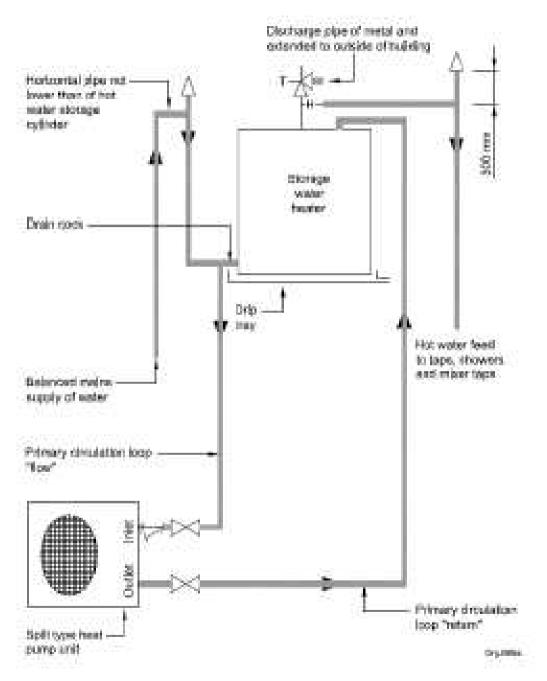


Figure 2 — Split type heat pump heat pump unit with an integrated pressure and temperature safety valve and but water outlet.

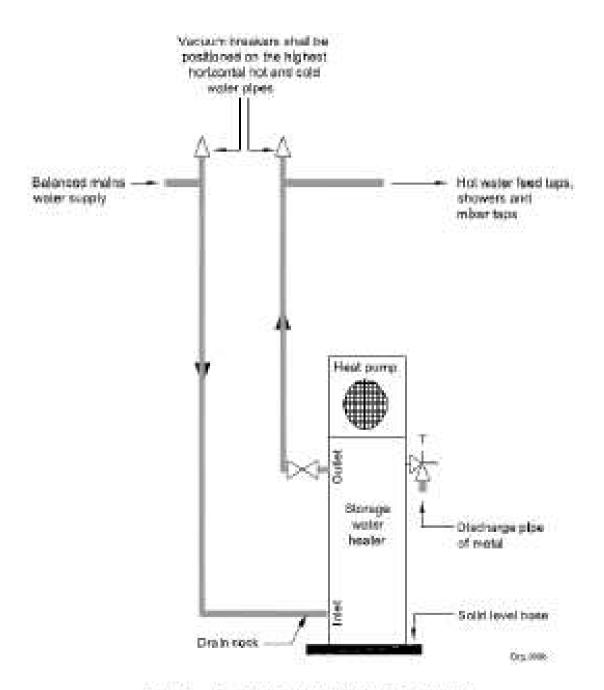


Figure 3 — Integral type heat pump unit (floor mounted)

CAUTION:

Most literature provided with domestic heat pumps state that a COP of 4 will be achieved if correctly installed.

Climatic conditions should be checked before a decision is made to install a heat pump.

The average ambient temperature to achieve the COP of 4 is stated as 20°C which is much higher than the average ambient temperature of most towns in SA.

For example, the average annual temperature in Cape Town is 17°C, and in Pretoria, 17.5°C

	Jan	Feb	Mar	Apr	Hay	Jun	Jul	Αυψ	Sep	0kt	Nov	Dec
Avg. Max Temperature	29	29	28	M	22 22	21	29	23	27	211	26	221
Avg. Min Temperature	17	17	16	12	7	9	3	7	11	14	15	16
Avg. Rain Daya	6	0.	4	3	II.	0	0	0	2	+	7	
Avg. Snow Days	ū	0	Œ	ū	đ:	0	σ	0	0	0	tr	D

Cape Tomi

	Jam	ridi	Mar	Apr	May	Jun	Jul	Ang	Sep	Oct	Nov	Dec
Avg. Temperature	10	20	19	16	14	22	n	12	10	16	17	200
Avg. Mae Temperature	17	26	26	25	21	19	16	19	20	19	24	26
Avg. Min Temperature	15	13	13	11	5	7	ō	7	ð	ш	12	15
Avg. Rain Days	3	2	3	+	7	9	9	3	7	6	5	
Dvg. Snow Deys	b	0	0	0	e	ō	0	a	n	b	0	0

5 Materials, pipes, fittings, components and fixtures

5.1 General

5.1.1 Materials, components, fittings and fixtures shall be so selected that they are suitable for the expected conditions of use.

5.1.2 If required, approval shall be obtained from the local authority regarding the use of specific materials or workmanship in the area concerned.

NOTE The schedule of approved products is normally the Joint Acceptance Scheme for Water Installation Components (JASWIC) acceptance list.

JASWIC ACCEPTANCE COMMITTEE WORKING LIST: ACCEPTED WATER COMPONENTS

Line	Product description	Manufacturer	Catalog reference	Specification	Mark/ comply	Seria
2	Cistem (close poupled)	Vaal Sanitaryware	Lonus 710013	SANS 821	Mari	475 ()
2	Cistem (close poupled)	Vaal Sanitaryware	Hibisous 710001:	SANS 821	Mark	470 (1
Ś	Cintern (concentral)	Gebert International AG	110.945	SANS 821	Mark	537 / 1
•	Distern (high level)	Dutton Plact on Eng	Eff (11 life)	SANS 821	Mark	6291
=	Discert (high level)	Outon Plant to Eng	Linc (15 litre)	SANS 821	Stark	673 /
n.	Distem (high level)	Parker Manufacturing	Puma (8 litres	SANS RZ1	Mark	WEI
ž	Cistom (high level)	Partier Manufacturing	Lynx (Differ & 11 (line)	SANS 821	MoA	4397
B	Cestern (cov level)	Outton Plast as Eng	Elf (11 litre)	SANS 921	Mark	6907
Ó	Cistem (jow level)	Dutton Plastics Eng	Loc (11 line)	SANS 821	Mark	274-1
tiĝi	Cistem (low level)	Parker Manufacturing	Pura (9 litre)	SANS 821	Mai	4481
13.	Ostern (low level)	Parker Manufacturing	Lynx (8 litre & 11 litre)	SANS 821	Mark	4387
12	Distant (low level)	Datton Plastics Eng	Alpha (91 tre)	SAMS 821	Blank	507
13	Clatert (low level)	Dutton Flastics Eng	National 9 libe Syphonic	SANS 821	Mark	254 (
94	Cistom (low level)	Dutton Plastics Eng	Superior	SANS 821	Mark	4107
15	Cistom (low level)	Vaal Santaryware	Hitisaus	SANS 821	Mark	470.1
18	Cistem (semi-high level)	Vaul Santaryware	Hitocus	SANS 821	Mark	478 /
17	Coupling (mechanical)	Thomas Pipe Products	Thomas Units Pipe Couplings	SANS(886-2	Comply	18207
ià.	Fitting (brank)(compression)	Actioner Enterprises Ltd.	Corrup compression fittings	SANS 1087H	Comply	1571 /
19	Fitting (brass) (compression)	Yuhuan Tongsin Pipe Co	Splashworks breas some fitting	SANS 100711	Mari	1606 (

JASWIC ACCEPTANCE COMMITTEE WORKING LIST: ACCEPTED WATER COMPONENTS

Line	Product description	Manufacturer	Catalog reference	Specification	Mark/ comply	Seria
520	Tap (various)	Colora Waterlesh (Pty) Ltd	Canna Senes	SANS 226/182	Mark	73 / 1
126	Tap (various)	Cobra Waterteen (Pty) Ltd	Crutch Series	SANS 220/18.2	Marx	8171
127	Tap (various)	Cobra Watemech (Pty) Ltd	Star Beries	SANS 226/182	Mark	1081 / 1
128	Tap (various)	Colors Watertesh (Pty) Utd	Non senes	SANS 226/2	Mark	398 / 1
20	Tap (various)	Cobra Watemech (Pty) Ltd	Capstan series	SANS 226/2	Mark	798 / 1
130	Tap (various)	Cobra Waterlech (Pty) Us	Gallauta senes	SANS 226/182	Mark	983 / 1
191	Тар (частоль)	Cobra Watertech (Pty) Ltd	Tudor Series	SANS 228/2	Mark	582 / 1
132	Tap (various)	Coora Wanertech (Pty) Ito	Stella Bright Series	SANS 220/2	Mark	00371
133	Tap (various)	Cobra Waterlech (Pty) Ltd	Stato Series	SANS 226/1/2	Mark	563 / 2
134	Tap (various)	ISCA (Ply) Ltd	ALP1	SANS 228/2	Mark	943 / 1
136	Tap (various)	ISCA (Pty) Ltd	Antica	SANS 226/2	Mark	043 / 3
138	Тар (часочь)	ISCA (Pty) Ltd	Windsor	SANS 226/2	Mark	945 / 4
187	Tap (various)	ISCA (Pty) Ltd	Palesa	SANS 226/2	Mark.	043 / 6
138	Tap (various)	ISCA (Pty) Ltd	Glassin	SANS 226/2	Mark	843 / 6
139	Tap (various)	Coors Waterteen (Pty) Ltd	Capstan Supreme series	SANS 220/182	Mark.	046 / 1
140	Tap (various)	Colora Watertech (Pty) Ltd	Matt Chrome 800 Series	SANS 226/2	Mark	046 / 2
141	Tap (various)	Colora Watertech (Pty) Ltd	Damara series	SANS 1480 & 226/2	Mark	P46 / 6
142	Tap (various)	Cobra Watertech (Pty) Ltd	Viotoriana Series	SANS 226/1/2	Mark	908 / 1
143	Tap (various)	Colora Watertech (Pty) Ltd	Metal senes	SANS 226/2	Mark	793 / 2

5.1.3 If it is desired or deemed necessary to use materials, components, fittings or fixtures not covered by this part of SANS 10252 or by an appropriate standard, proof of quality and performance of the material or workmanship shall be established by tests or by reference to other appropriate standards.

PRESENTER'NOTE:

The designer needs to prove that the product complies with the minimum testing standards as per the applicable SANS standard.

5.1.4 The following factors shall be considered when materials, components, fittings and fixtures are being selected:

- a) life cycle costs;
- b) effect on water quality;
- c) internal and external corrosion;
- d) compatibility of different materials;
- e) aging, fatigue and temperature effects;
- f) mechanical properties;
- g) durability;
- h) availability;
- i) water quality; and
- j) dezincification resistance.

- 5.1.5 All materials, components, fittings and fixtures in every part of a water installation shall
- a) operate effectively under all normal conditions likely to be experienced when the water installation is in service, and
- b) withstand, without damage or deterioration, sustained temperatures of
 - up to 40 °C in the case of cold water installations, and
 - 2) up to 60 °C and occasionally up to 100 °C in the case of hot water installations (in order to allow for malfunctions of heated water fittings or components) or to allow for periodic high temperature flushing as part of Legionella control regimes.

5.1.6 Selected fittings or components or any other apparatus shall not induce pressure surges that can cause damage to any part of the water installation.

NOTE Quick-closing valves and pressure booster pumps can (for example) induce undesirable pressure surges in a water installation unless special measures are taken to absorb such surges

5.1.7 Materials selected for the manufacture of purposemade water heaters and storage containers shall be compatible with the quality of the water to be heated or to be stored, and shall comply with the relevant details given in the appropriate of 5.2. 5.1.8 All rubber components that are in contact with potable water, such as joint rings, tap washers and flange packings, shall, in order to control the multiplication of Legionaella pneumophila bacteria in water installations, be of a composition that will not promote microbiological growth.

Rubber joint rings that comply with the relevant requirements of SANS 4633 and that have the dimensions, composition and hardness that are suitable for the particular application, shall be deemed to be acceptable.

5.2 Pipes and pipe fittings

NOTE 1 Piping materials used for water installations in buildings include, but not limited to galvanized mild steel, copper, stainless steel, polypropylene, polyethylene, cross-linked polyethylene, PVC-u, chlorinated PVC).

NOTE 2 Metals and metal alloys (such as copper and stainless steel) that rely on the presence of protective surface films for their corrosion resistance are particularly at risk to pitting corrosion under unfavourable conditions.

NOTE 3 Where galvanized mild steel pipes and copper pipes are used in the same system, the corrosion rate of galvanized steel is usually substantially increased by the traces of copper present in the water. Dissolved copper ions can stimulate the corrosion of zinc coatings and bare steel surfaces, either by direct electrochemical exchange reactions or by galvanic attack. Dissolved copper is, however, usually only found in cases where galvanized mild steel hot water outlet pipes are used together with copper domestic water heaters that operate at excessively high temperatures.

NOTE 4 Where galvanized mild steel pipes and copper pipes are to be used in the same system especially at temperatures in excess of 60 °C, it is recommended that the copper pipe is downstream to the galvanized steel pipe.

5.2.1 Copper and copper alloy

- 5.2.1.1 All copper alloy components in contact with potable water shall comply with the minimum standard when tested in accordance with SANS 6509. The maximum penetration shall not exceed 250µm.
- 5.2.1.2 Notwithstanding the requirements in 5.2.1.3, the following shall be deemed to be acceptable:
 - a) copper tubes recommended in SANS 460 for the design conditions;
 - b) solders, fluxes and the method of soldering described in SANS 460; and
 - c) copper-based fittings for copper tubes that comply with the requirements of SANS 1067-1or SANS 1067-2, as relevant.

SANS 460 Class 0:

A hard drawn thin-walled tube for use without bending, and recommended for above ground use only. Hard drawn tubing is not recommended for underground use due to its thin wall and lack of flexibility. Any change of direction using SANS 460 Class 0 should be made using capillary fittings and not compressive fittings.

Local annealing in order to produce a bend, offset or crossover is not recommended. Oxyacetylene brazing of SANS 460 Class 0 using capillary fittings is not recommended.





SANS 460 Class 1:

A half hard thin-walled tube for above ground use only. This tube can be bent using a bending tool with inner and outer formers. Spring bending is not advised due to the spring being too loose in the tube and the walls of the tube collapsing. SABS 460 Class 1 - 28mm to 108mm is ideally suited for the drawing of "T" joints.

SANS 460 Class 2:

A half hard, heavy gauge tube with excellent bending qualities. This class is also used underground under normal conditions i.e. non-aggressive soils. This is the only class that can be bent by using an Internal Bending Spring. Care should be taken when installing tube underground. The tube should be protected against external corrosion using CXP tape. SABS 460 Class 2 - 28mm to 108mm is ideally suited for the drawing of "T" joints



SANS 460 Class 3:

This class is a heavy, thick walled, half hard copper tube with excellent bending qualities, designed specifically for underground use where soil movement takes place. Care should be taken when installing tube underground and it should be protected against external corrosion using CXP tape.

5.2.1.3 Unless the water is suitably treated, copper piping shall not be used where

- a) the water can so dissolve an undue amount of copper that an unacceptable green staining is produced, or
- b) copper deposits onto aluminium or zinc surfaces will promote galvanic attack.

5.2.1.4 Copper or copper alloy pipes and fittings shall not be used, unless suitably protected against external corrosion, where they might be in contact with materials such as

- a) ash,
- b) sodium chloride (salt),
- c) ammonia, or
- d) any compound that consistes of of magnesium oxychloride (magnesite).

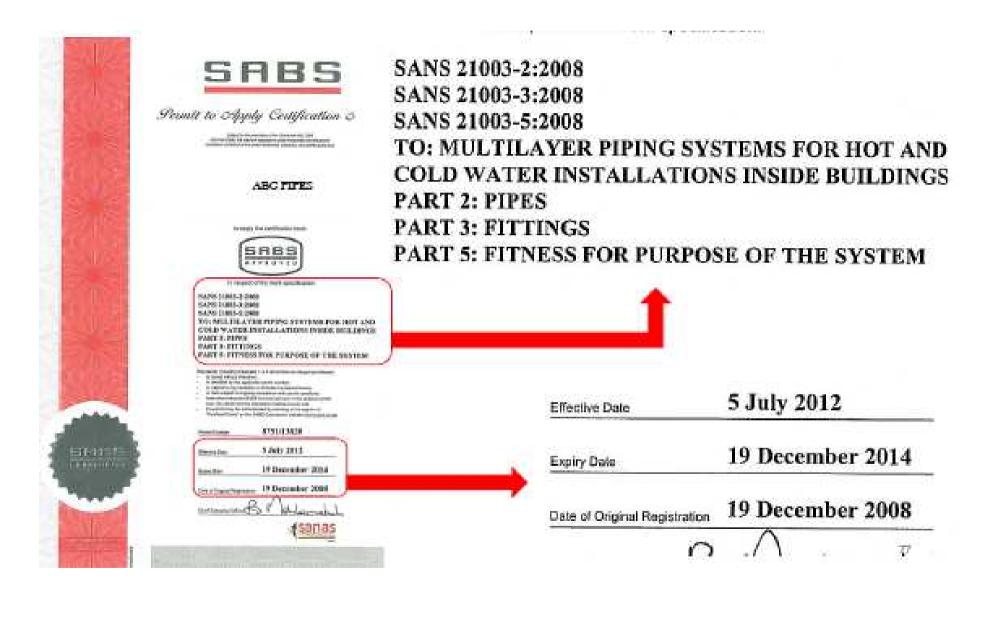
- 5.2.3.7 Plastics pipes and fittings for hot and cold water supply systems shall comply with one of the following standards:
 - a) for PE-X (cross- linked polyethylene): SANS 15875 1, SANS 15875-2, SANS 15875-3 and SANS 15875-5;
 - b) for PB (polybutylene): SANS 15876-1, SANS 15876-2, SANS 15876-3 and SANS 15876-5;
 - c) for PVC-C (chlorinated polyvinyl chloride): SANS 15877-1, SANS 15877-2, SANS 15877-3 and SANS 15877-5;
 - c) for PE-RT (raised temperature cross linked polyethyelene): SANS 22391-1, SANS 22391-2, SANS 22391-3 and SANS 22391-5; and
 - d) for PE-X Multi-layer piping systems: SANS 21003-1, SANS 21003-2, SANS 21003-3 and SANS 21003-5.

- 5.2.3.8 The minimum rating of a polymer pipe used in hot and cold water systems in buildings is class 2, PN16 at 20 °C, 8 bar at 70 °C, and shall be marked as such on the pipe.
- 5.2.3.9 Algae growth can occur in plastics pipes if there is any translucence. Plastic pipes on hot and cold systems shall only be used inside buildings.
- 5.2.3.10 For pipes and fittings, guidance on the application of the system shall be found in SANS 4427-5, SANS 15874-5, SANS 15875-5, SANS 15876-5, SANS 15877-5, SANS 22391-5 and SANS 21003-5. Any plastic piping systems for hot water use shall be class 2 (70 °C operating temperature), and shall have a minimum operating pressure (M.O.P) of 600 kPa (6 bar) at 70 °C.

All SANS standards for plastic polymer piping system for hot and cold water supplies are approved for use inside buildings only. All plastics pipes used in hot and cold water installations near external doorways and windows, shall be protected from sunlight.

Unlike metal pipes (steel and copper) that have generic pipe and fitting standards, thermoplastic pipe systems are required to be installed using the fittings and tools that are tested and approved as a complete system, The use of pipes, fittings and tools from other manufacturers or suppliers, that are not the same as the approved system, shall not be acceptable.





5.2.5 Iron and steel

5.2.5.1 The following shall be deemed to be acceptable:

- a) malleable cast-iron pipe fittings that comply with the requirements in SANS 14;
- b) ductile iron pipes that comply with SANS 1835;
- c) steel pipes and pipe fittings with a nominal bore up to 150 mm that are suitable for screwing, in accordance with SANS 1109-1 pipe threads, and that comply with the requirements in SANS 62-2;
- d) galvanized steel tubes, tubulars and fittings that have been galvanized in accordance with the requirements of SANS 32; and
- e) steel pipes and fittings that comply with the requirements of SANS 62-1, SANS 719, SANS 815-1 and SANS 815-2, as applicable.

5.2.5.2 Where buried galvanized steel tubes and fittings can suffer rapid corrosion in acidic soils, special precautions shall be taken to protect such pipes and fittings against external corrosion.

Several coastal local authorities do not allow the use of galvanized steel pipes in water supply installations.

5.3.3 Taps, mixers and showers

5.3.3.1 Taps and mixers

5.3.3.1.1 Metallic water taps and mixers shall comply with the requirements in SANS 226, SANS 1480, SANS 1808-9, SANS 1808-16, SANS 1808-30, SANS 1808-35, SANS 1808-37, or SANS 1808-66, as relevant.

5.3.3.1.2 Draw-off taps shall operate effectively at the internal water pressure recommended by the manufacturer.

5.3.3.1.3 Plastics taps shall comply with SANS 1021.

5.3.3.2 Showers

Showers shall be of a type that can operate effectively at the internal water pressure recommended by the manufacturer.

8.6.3 Pipes laid in or through floors, concrete slabs or walls

- 8.6.3.1 Where any portion of a pipe is concealed in a floor, concrete slab or wall, the following shall apply:
 - a) adequate measures shall be taken to protect such portion from external pressure or from the transmission of any load to it;
 - should a leak develop in such portion, the installation shall be such that the portion of the pipe can be removed without danger to the building structure; and
 - c) plastics pipes shall not be rigidly encased in floors, concrete slabs or walls.

- 8.6.3.2 Where any portion of a pipe passes through a wall or under a floor, such portion should preferably be installed inside a sleeve of internal diameter of at least 15 mm plus the outside nominal diameter of such portion (see figure 15 and figure 16).
- 8.6.3.3 Pipes installed within a cavity wall shall be securely fixed. No pipe shall pass through concrete expansion or concrete joints, unless acceptable provisions have been made to the pipework for movement.

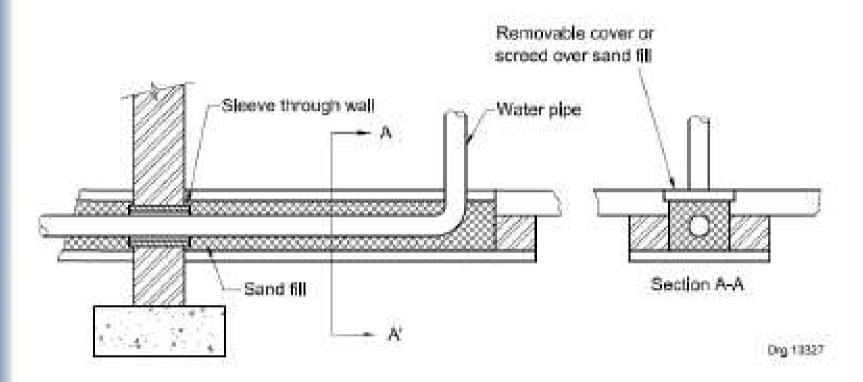


Figure 15 — Example of a duct for installing a water pipe within a surface slab or a floor

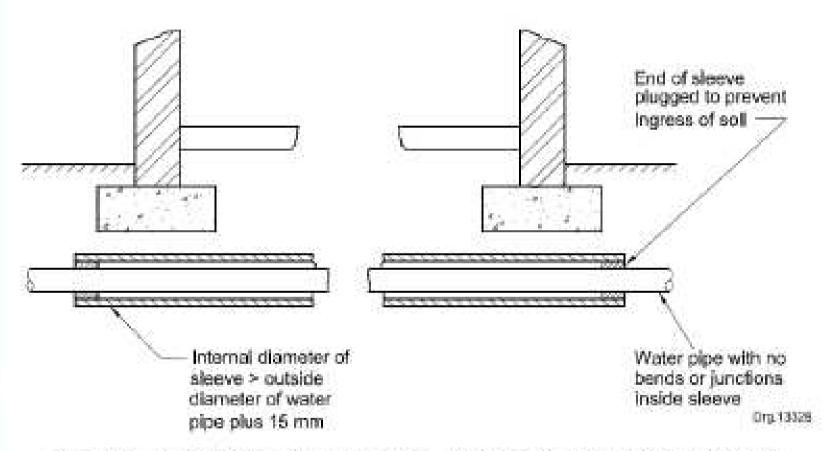


Figure 16 — Sleeve for installing a water pipe under a building or under a surface slab

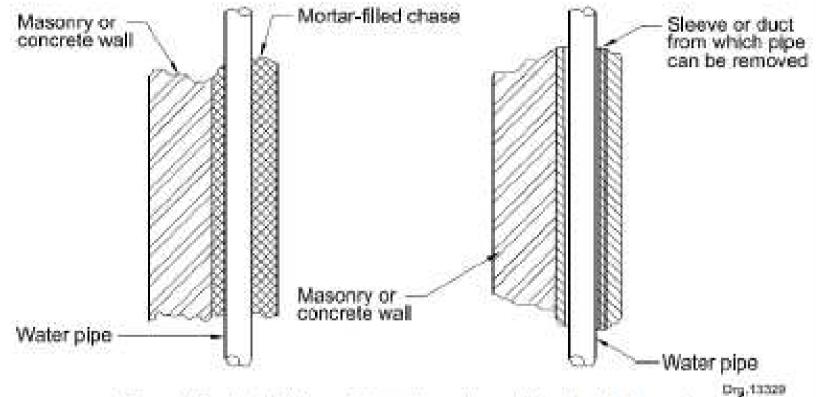


Figure 17— Installation of pipes in walls and structural elements

WATER SYSTEM:

- "Volume" is related to the number of people
- "Flow" is related to number of fixtures simultaneous use
- Size of piping relates to Q_p = (∑Q)^N

4.2.2 Probable (or design) flow demand

4.2.2.1 The probable water flow demand for pipes in installations without automatic shut-off flush valves shall be calculated using the following equation:

$$Qp = (\Sigma Q)^n$$

Where

Qp is the probable flow demand, in litres per minute;

ΣQ is the arithmetic sum of the design flow rates of all the individual fittings supplied by the pipe (see table 3 for design flow rates), in litres per minute; and

n is a factor related to the probable simultaneous use of the fittings. Values of n are given in table 4.

4.2.2.2 The probable water flow demand for pipes in installations with low-pressure automatic shut-off flush valves shall be calculated using the following equation:

$$Qp = (\Sigma Q)^n + 80$$

4.2.2.3 The probable water flow demand for pipes in installations with high-pressure automatic shut-off flush valves shall be calculated using the following equation:

$$Qp = (\Sigma Q)^n + 45$$

4.2.2.4 The probable water flow demand for pipes in installations where all the fittings supplied by a pipe would probably operate simultaneously (automatic shutoff flush valves excluded) shall be calculated using the following equation:

 $Qp = \Sigma Q$

4.2.2.5 Equation (4) can be used in all cases for the final two fittings (automatic shut-off flush valves excluded) supplied by a branch pipe. Working upstream from this branch, the calculated value of Qp shall be retained until it is replaced by a new value obtained from using equation (1), (2) or (3).

Table 3 — Flow rates from terminal water fittings

1	2	3	4	5
Sanitary fixture or fitting	Likely maximum flow rate per tap or fitting ^a	Likely minimum flow rate per tap or fitting	Design flow rate per tap or fitting	Design flow pressure at tap or fitting for design flow rate ^b
	L/min	L/min	L/min	kPa
Wash-hand basin				
15 mm taps (plain outlet)	25	5	10	10
15 mm taps (aerated outlet)	12	5	8	50
Mixer (plain outlet) (hot and cold separately)	25	5	10	15
Mixing valve (aerated outlet) (hot and cold separately)	12	5	9	50
15 mm taps (public facility) (flow controlled)	6	3	4	20
Bath				
15 mm taps (plain outlet)	30	12	15	15
20 mm taps (plain outlet)	40	20	25	15
20 mm taps (aerated outlet)	20	12	12	50
Mixer (plain outlet) (hot and cold separately)	40	12	25	15
Mixing valve (aerated outlet) (hot and cold separately)	25	15	20	50 ⁹¹

Table 3 — Flow rates from terminal water fittings

Shower (wall mounted)				
Showerhead (standard) (hot and cold combined)	30	8	15	20 - 50
Showerhead (water saving) (hot and cold combined)	12	6	10	50 100
Water closet ^a	-			
Cistem float valve		3	5	100*
Automatic shut-off flush valve (low-pressure pattern)	Ê	-	110°	30 - 50°
Automatic shut-off flush valve (high-pressure pattern)	-	-	65*	150 - 200°
<u>Urinal</u>				
Siphonic type (automatic shut- off flush valve)	12	929	60	30
Wash-down type (automatic shut-off flush valve)	<u>.</u> 2	929	10	50
Bidet				
Mixer or mixing valve (hot and cold separately or combined)	12	5	9	50

Table 3 — Flow rates from terminal water fittings

1	2	3	4	Design flow pressure at tap or fitting for design flow rate	
Sanitary fixture or fitting	Likely maximum flow rate per tap or fitting	Likely minimum flow rate per tap or fitting	Design flow rate per tap or fitting		
	L/min	L/min	L/min	kPa	
Sink					
15 mm taps (plain oulet)	25	6	12	15	
20 mm taps (plain outlet	35	15	20	15	
Mixer (plain outlet) (hot and cold separately)	25	10	15	15	
Mixing valve (serated outlet) (hot and cold separately)	12	6	10	50	
Wash trough					
15 mm taps (plain outlet)	25	6	2	15	
15 mm taps (aerated outlet)	12	6 5	2 8	50	
20 mm taps (plain outlet)	35	10	15	15	
20 mm taps (aerated outlet)	20	10	12	50	
Mixer (plain outlet) (hot and cold separately)	25	10	15	15	
Mixing valve (aerated outlet) (hot and cold separately)	12	6	10	50	

Table 3 — Flow rates from terminal water fittings

Storage tank				
15 mm float valve (3 mm seat bore)	8	3	5	100
15 mm float valve (5 mm seat bore)	18	6	12	100
20 mm float valve (6 mm seat bore)	30	10	20	100
25 mm float valve (10 mm seat bore)	70	23	50	100
38 mm float valve (19 mm seat bore)	200	90	200	100
50 mm float valve (25 mm seat bore)	500	160	330	100
Taps				
15 mm (plain outlet)	25	6	15	15
20 mm (plain outlet)	35	10	25	15

^{*} The likely maximum flow that the user of the fixture or fitting would normally allow the tap or fitting to discharge, and not necessarily the maximum flow rate attainable from the tap or fitting.

* Values to be used where the flow-pressure curve for the tap or fitting is not available from the manufacturer.

Design flow rates for WC pans should preferably be about 120 L/min for maximum flushing efficiency.

The cistem float valve can operate at lower pressures.

Where a pipe supplies several low-pressure automatic shut-off flush valves, calculate the cumulative flow (Q), using the following flow rates:

1st valve 110 L/min, 2nd valve 85 L/min, 3rd valve 65 L/min, 4th valve 45 L/min, 5th valve 20 L/min, all valves thereafter 5 L/min each.

Where a pipe supplies several high-pressure automatic shut-off flush valves, calculate the cumulative flow (Q), using the following flow rates:

1st valve 65 L/min, 2nd valve 55 L/min, 3rd valve 45 L/min, 4th valve 35 L/min, 5th valve 25 L/min, all valves thereafter 5 L/min each.

Minimum flow pressure.

Table 3 — Flow rates from terminal water fittings

Storage tank				
15 mm float valve (3 mm seat bore)	8	3	5	100
15 mm float valve (5 mm seat bore)	18	6	12	100
20 mm float valve (6 mm seat bore)	30	10	20	100
25 mm float valve (10 mm seat bore)	70	23	50	100
38 mm float valve (19 mm seat bore)	200	90	200	100
50 mm float valve (25 mm seat bore)	500	160	330	100
Taps				
15 mm (plain outlet)	25	6	15	15
20 mm (plain outlet)	35	10	25	15

^{*} The likely maximum flow that the user of the fixture or fitting would normally allow the tap or fitting to discharge, and not necessarily the maximum flow rate attainable from the tap or fitting.

Values to be used where the flow-pressure curve for the tap or fitting is not available from the manufacturer.

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Where a pipe supplies several high-pressure automatic shut-off flush valves, calculate the cumulative flow (Q), using the following flow rates:

1st valve 65 L/min, 2nd valve 55 L/min, 3rd valve 45 L/min, 4th valve 35 L/min, 5th valve 25 L/min, all valves thereafter 5 L/min each.

Minimum flow pressure.

7.7.1.3 Unless otherwise stated, the length of an unheated pipe (dead leg) conveying water direct from a fixed water heater to a terminal water fitting, or from the point of take-off from a hot water circulating system to a terminal water fitting, shall be such that the internal volume of that pipe does not exceed 4ℓ. The internal volume of pipes and permissible lengths in terms of the 4ℓ volume limit are given in table 19 and recommended limits are given in table 20.

Table 19 - Internal volume of pipes

1	2	(3)	4
Type of pipe	Nominal diameter	internal volume	Length of pipe containing 4 L of water
	mm	L/m	m
Galvanized mild steel (medium)	15 20 25 32	0,196 0,356 0,581 1,012	20,4 11,2 6,9 4,0
Copper (class O)	15 22 28 35 42 54	0,150 0,330 0,547 0,835 1,232 2,091	26,7 12,1 7,3 4,8 3,2 1,9

NOTE. Apart from the volume limit, more than just the internal volume of the pipe might have to be run to waste before water of sufficient temperature emerges from the tap, since the hot water has to heat up the pipe. For example, a tap in a wash basin supplied by a 15 mm diameter galvanized mild steel pipe 12 m in length and discharging at a rate of 6 L/min, would have to run for 1 min to 2 min before the temperature of the water entering the basin is adequately hot. Thus, the volume of water run to waste would be 6 L to 12 L, whereas the actual internal volume of the pipe is only 2,4 L. The designer should therefore attempt to ensure that where practicable, the lengths of such pipes are well below those given in column 4 of this table.

Table 20 — Recommended maximum lengths of dead-leg piping from a storage heater, or from the point of take-off from a hot water circulation system to a terminal water fitting

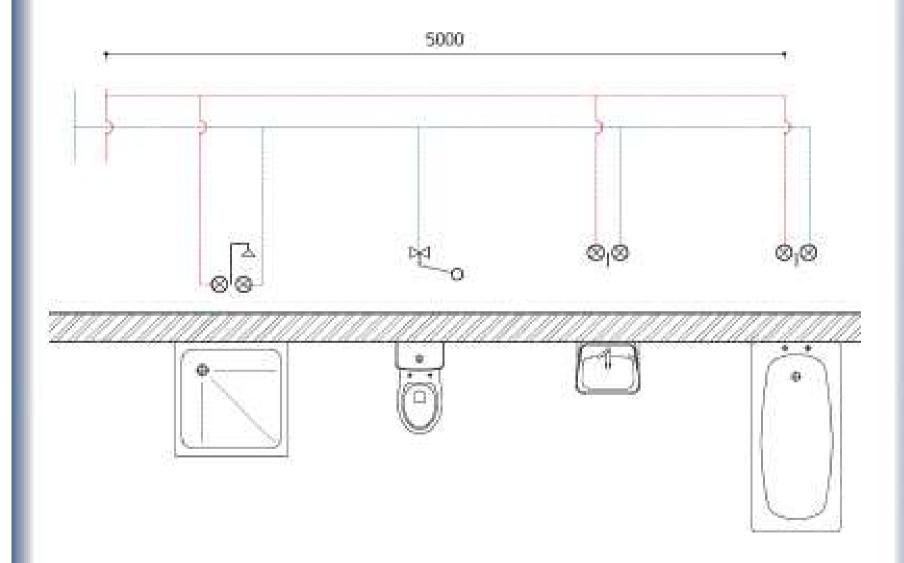
1	2	
Internal diameter of pipe	Maximum lengtl of pipe	
mm	m	
≤ 19	12	
> 19 and ≤ 24	8	
> 24	3	

Table 4 - Values of nº

i1	2
Nature of use of building	Value of na
Dwellings (economic)	0,5 - 0,70
Dwellings (low-cost)	0,5 - 0,75
Offices	0,5 - 0,70
Shops	0,5 - 0,70
Hostels	0,75 - 0,80
Public facilities	0,75 - 0,80
Kitchens	0,70 - 0,80
Hotels	0,5 - 0,75
Factory ablutions	0,75 - 0,80
Day school ablutions	0,5 - 0,80

In large installations, the value of n adopted for the main supply pipes shall, in general, be less than that adopted for branch pipes. Where the flow exceeds 50 000 L/min, the value of n shall not exceed 0,7.

EXERCISE



DESIGN FLOW RATES (Table 3)

2 - 2

Showerhead (standard)
Cistern float valve
Wash-hand basin mixer
Bath mixer

158/min 58/min 108/min 258/min

COLD WATER

Qp = $(\Sigma Q)^n$ = $(15 + 5 + 10 + 25)^{0.7}$ = $55^{0.7}$ = $16,53\ell/min$

HOT WATER

Qp =
$$(\Sigma Q)^n$$

= $(15 + 10 + 25)^{0.7}$
= $50^{0.7}$
= $15,46\ell/min$

The flow rate required for the bath mixer is 25t/min which is more than 16,53t/min or 15,46t/min
Use 25t/min

Go to manufacturer's data

TABLE 1 Comparison between SANS 46-0/0 copper tube (Cu) and Polypropylene (PP) showing bare area, percentage difference and comparative flow rates.

Hominal Tube Size (mm)	thick	el well oness mil	71000	ea mess	Copper's greater unes (%)	ut 2.5	ite (1/m) im/sec m2)	kpa p	o drop is se I dro gdi
	PP	6	199	Ú	36,767	PF	fa	39	G
15	1.8	0.5	102	154	50	15.5	22.0	88,0	55.0
22	2.7	0.6	216	346	60	32.	52.0	6.5	33.5
28	3.4	0.6	35.3	546	59	53.0	4	41.0	24.5

Ø22 ND Class 0 Copper

The total length of the dead leg (hot water) is less than 8m (Table 20) – less than 4ℓ of water will be wasted before water is hot at tap - therefore no HWR required. In the case of dwelling houses, it will usually not be necessary to carry out a detailed exercise to size the pipes for the installation. For the internal hot and cold water supply systems, certain basic pipe sizes will be generally applicable.

The service pipe between the boundary and the house should be sized.

Where automatic shut-off flush valves are used in lieu of cisterns for WCs, it will be necessary to size the pipes supplying such valves.

Table F.1 — Recommended pipe sizes for in-house installations that incorporate a mains-fed of a type 3 standard water heater (see SANS 151)

1	2	3			
	Pressure rating of water heater				
Pipe	Not exceeding 200 kPa	Exceeding 200 kPa			
	Recommended pipe size (average internal diameter)				
Branch from service pipe to water heater					
Cold water feed to first branch	Larger of 19 mm and the	Smaller of 19 mm and the service pipe			
Hot water feed from water heater to first branch	service pipe				
All other pipes					

Pressure rating of pressure control valve controlling supply to water heater exceeds 200 kPa.

The recommended pipe sizes for installations that incorporate a storage tank and a type 3 standard water heater as given in SANS 151, are given in table F.2.

Table F.2 — Recommended pipe sizes for installations that incorporate a storage tank and vented water heater

T.	2		
Pipe	Recommended pipe size (nominal internal diameter) mm		
Branch from service pipe to storage tank	13 to 19		
Cold water feed from service pipe to first branch	Smaller of 19 and the service pipe size		
Pipe from storage tank to water heater	19 10 21		
Low-pressure cold water feed to first branch	13 to 19		
Hot water feed from water heater to first branch and vent	19 to 21		
All other pipes	13 to 19		

Residual water pressure in our domestic water systems is determined by gravity, pipe size, elevation, water volume and distance from source.

Residual water pressure is defined as the water pressure in the line when water is flowing, as opposed to static pressure, which is the pressure of the water when it is not flowing.

In cases of domestic demand (how water gets into our home), water pressure is never static because the system is always being drawn on from somewhere.

Drag and pipe friction reduces residual water pressure. This is the same as any other material traveling by another. Think about dragging your feet across the floor. It requires more effort to drag your feet across the floor than it does to lift them through the air. This is because there is less friction and drag in the air than on the solid floor.

Most domestic water supply systems use gravity to maintain water pressure and deliver water to homes. If residual water pressure is low, it could be caused by a low volume of water in the system, pipes being clogged and pipes that are too small. Pipes that are too small reduce the amount of pressure that can travel through the system. Long periods of small pipes in a system will reduce the volume of water passing through, making water pressure drop regardless of the strength of supply pressure.

Another determination of residual water pressure is elevation. It is a given that it would take more pressure to run water uphill, and the further away from the pressure source you are, the more your elevation will affect your water pressure.

1 atm (Atmosphere) = 101 300 Pa (101.3kPa)

= 1.013 Bar

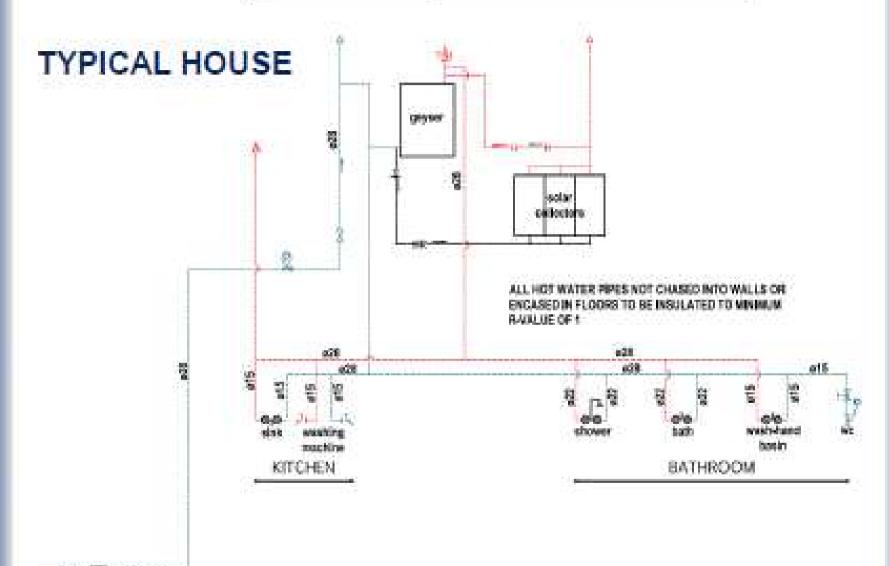
= 14.7 psi

= 10.3m water

= 760 mm Hg

#15 - #GB CONNECTION HDPE UNDER GROUND





AREA	FIXTURE	STANDARD	DESIGN FLOW RATE
KITCHEN	Sink mixer plain outlet hot and cold separately	226	15
	Tap (plain outlet)	226	15
	Tap (plain outlet)	226	15
BATHROOM	Shower mixer standard	226	15
	Bath mixer standard	226	15
	Wash-hand basin mixer standard hot and cold separately	226	10
	Cistern	821	5

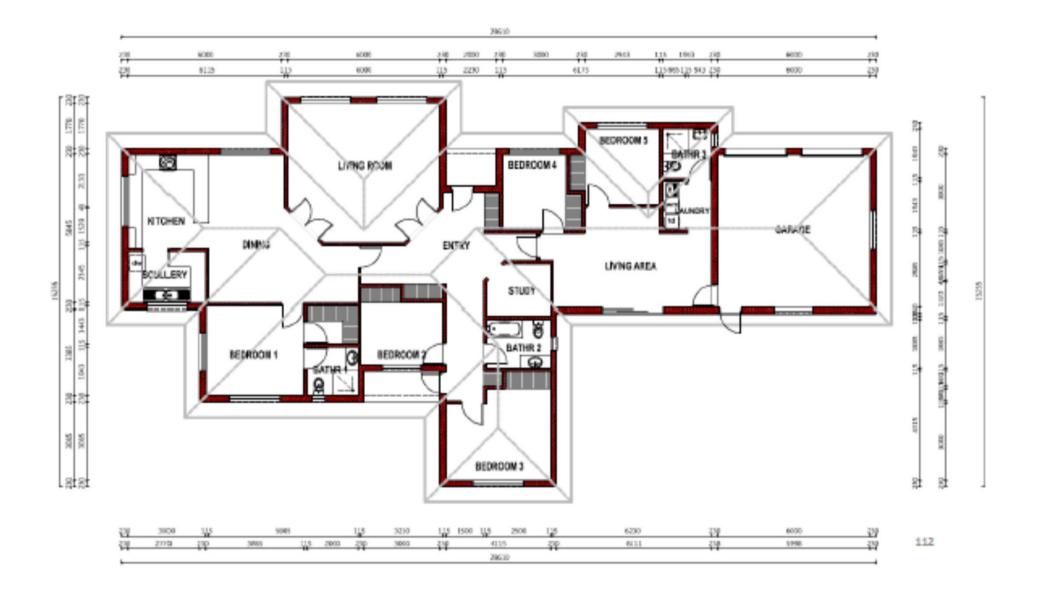
EXERCISE

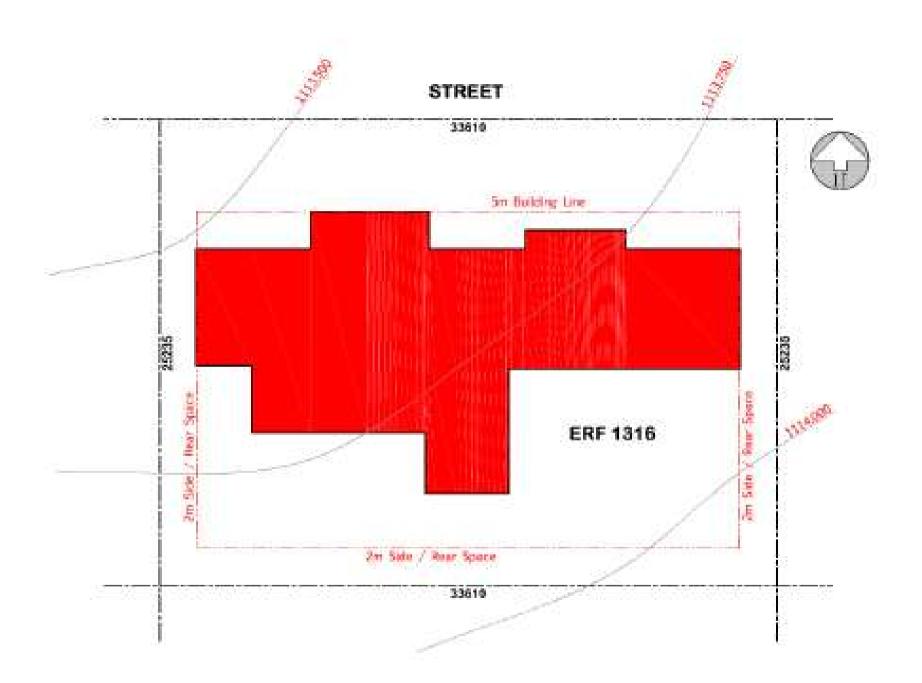
Typical dwelling

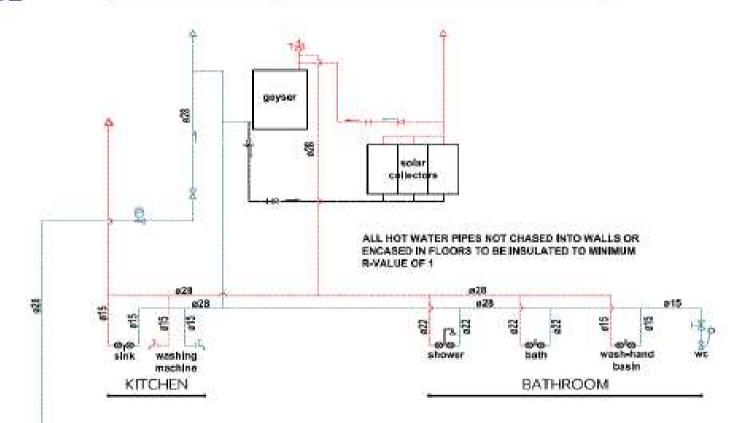
- 5 bedrooms
- 3 bathrooms
- 1 kitchen
- Laundry
- Scullery

Solar geyser(s) with electrical backup element will be used.

- Determine the capacity of the storage required for a efficient installation.
- 2. What will be the minimum storage capacity required to satisfy Regulation XA2?
- 3. Provide a schematic water reticulation layout plan.







#15 - #28 CONNECTION HDPE UNDER GROUND A20 Classification: H4

A21 Occupancy: 2 persons/bedroom

Type of hot water generation: Solar with back-up element

Hot water demand (SANS10252-1): 140ℓ per day per person

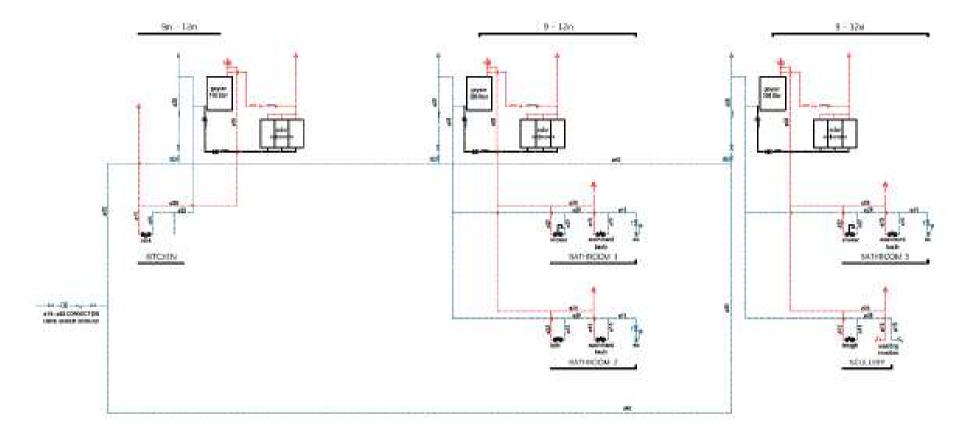
Number of Bedrooms: 5

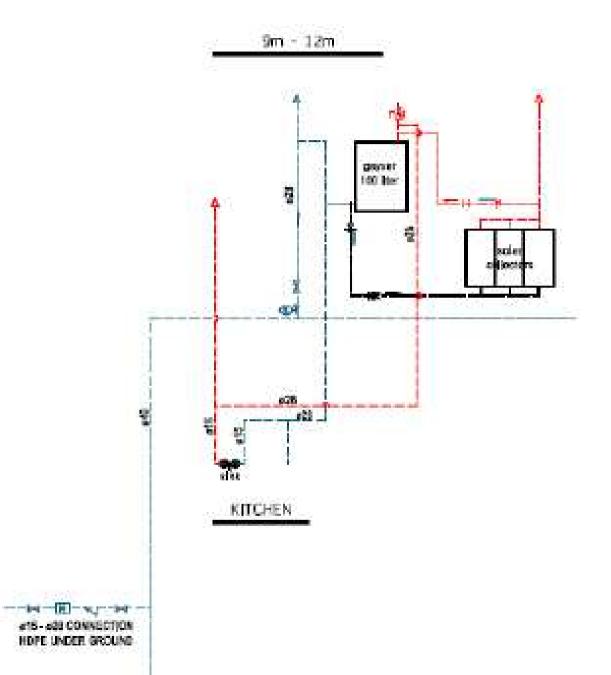
Total demand: $5 \times 2 \times 140 = 1400$

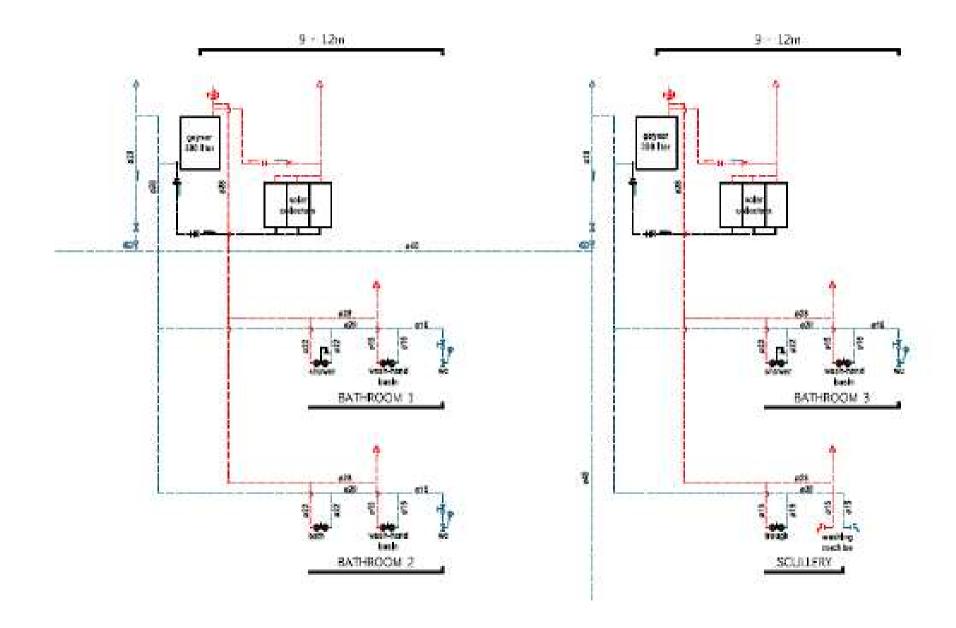
Hot water storage capacity required: 1400 × 50% = 700%(50% XA2)

Capacity provided: 300ℓ + 300ℓ + 100ℓ

	1000000	1000000	T	37.53
	Wilhe	201ee	881 te	\$31 lite
Sylvater Materials	Thereins send he high promises	The line and to hip pressure I	Decima steel to high procure	The time word for high process
	Mark MI, 14,965	Mark Art, 18 yes	NUMBER OF LINES	(Hally \$21, 1.0-mg)
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Plumbing Certificate of Compliance



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PLUMBING COC

- The Plumbing Industry registration Board CoC is a system and process whereby a licensed plumbing practitioner will self-certify their plumbing work by issuing of a plumbing certificate of compliance to the relevant owner, municipality, local authority and/or insurance company. Through the process the licensed plumber shall take ownership for their plumbing work and be held accountable for the said works.
- Plumbing Certificates of Compliance are issued by licensed plumbers to certify that their plumbing work complies with all regulatory installations requirements.

- A plumbing certificate of compliance will be issued for most plumbing work, including:
 - Where the total value of work, including materials, labour and VAT, is more than R1500.00 (material costs must be included, regardless of whether the materials were supplied by another person)
 - The installation, relocation or replacement of any Electric Water Heating System, regardless of the cost
 - For every separate installation on a site.

- A plumbing certificate of compliance will be issued for most plumbing work, including:
 - The construction, installation or alteration of any above or below ground sanitary drain; regardless of the cost
 - The installation, relocation or replacement of any Hot Water Solar Water Heating System
 - The installation, relocation or replacement of any Heat Pump Water Heating System

- A Plumbing certificate of compliance shall be issued to the relevant owner with five working days of the completion of the said plumbing works. Only a licensed plumber may purchase and issue compliance certificates.
- It is illegal for any person who works on plumbing installation if he/she is not a qualified plumber or not working under the adequate supervision of a qualified plumber. Registered persons under the category of qualified plumbers are qualified plumbers and may carry out plumbing works and may supervise non-qualified plumbers or plumbing learners, however they will not be allowed to purchase or issue Plumbing Certificate Compliance for plumbing installations.

WATER RETICULATION IN BUILDINGS

FIRE INSTALLATIONS

4.1 General

The functional regulation W3 contained in part W of the National Building Regulations shall be deemed to be satisfied where

- a) fire installations comply with the requirements of 4.2, 4.3, 4.4 and 4.5,
- a supply of water is provided in each division for the effective operation of the number of hose reels, hydrants and sprinkler heads that are required in accordance with SANS 10400-T and which may be operated or come into operation simultaneously, and

- c) the fire installation is either
 - the subject of a rational design prepared by a competent person (wet services) or a competent person (fire engineering) in accordance with the general principles and requirements contained in SANS 10252-1 and, if relevant, SANS 10287, or
 - 2) in accordance with the requirements of 4.6 where the area in which the building is located is serviced by a fire brigade, contains no sprinkler system, and serves not more than three fire hydrants in a division.

4.2 Communication pipe

A fire installation shall be connected to a communication pipe provided by the local authority and located at a position and depth as determined by such local authority.

4.3 Water meter

Where so required by the local authority, provision shall be made in a fire installation for the supply and installation, by the local authority, of a water meter. Such meter and any related valve(s) shall not significantly restrict the flow of water.

4.4 Isolating valves

An isolating valve shall be fitted in a fire installation at a position that is not more than 1,5 m inside the boundary of the site, and shall be clearly marked as such.

4.5 Fire pump connections

4.5.1 In any fire installation

- a) any pipe which serves any hydrant or an automatic sprinkler installation, shall be provided with a twin pumping connection; and
- b) any pipe fitted with one or more fire-pump connections, unless such pipe discharges directly into a storage tank, shall be fitted with a pressure gauge reading up to 2 500 kPa and a non-return valve so located as to shut off automatically the direct supply of water from the local authority system to such installation whenever and for so long as any such fire pump connection is in use.

4.5.2 Any pumping connection shall be

- a) situated in a readily accessible position outside the building at ground level,
- b) mounted on the face of the building in an accessible position, and
- c) clearly marked as such.
- 4.5.3 No non-return valve in a fire installation shall be so positioned as to prevent or hinder the flow of water from a fire-booster connection to a fire installation.

4.6 Pipework

4.6.1 In any fire installation

- a) the nominal diameter of
 - a communication pipe serving such installation shall be not less than 75 mm,
 - a service pipe supplying water to a fire hydrant shall be not less than 75 mm, and
 - a service pipe supplying water to a hose reel installation shall be not less than 25mm;

- b) the pressure head (PF), when calculated in accordance with the following formula, shall equal or exceed
 - at any hose reel within a building or any division within a building: 30 m
 - 2) at the fire pump connection: 5 m

PF ≥ PM - (HF - HC) - PL

where:

PM is the static pressure head, in metres, at the juncture between the communication pipe and the service pipe, and which, unless otherwise directed by the local authority, is the minimum head measured at a point in time;

HF is the elevation of the fire pump connection or hose reel, in metres, above a common datum (see figure 1);

HC is the elevation of the communication pipe at the juncture with the service pipe, in metres, above or below, or on the same level as the common datum (see figure 1). If the elevation is below the common datum, the volume between HF and HC shall be added and not subtracted:

PL is the sum, in metres, of all the products of the length of service pipe of a particular diameter serving the fire pump connection or hose reel, and the friction factor obtained from table 1 based on the following:

- a) fire hydrants: the simultaneous use of all hydrants within a division; or
- b) fire hose reels: the simultaneous use of all fire hose reels within a division.

- 4.6.2 All fire installation pipework shall be constructed in accordance with the relevant requirements of SANS 2001-DP2 or SANS 2001-DP6 and shall have a pressure rating of not less than 1 200 kPa.
- 4.6.3 All fire installation pipework installed above ground or within the structure of a building shall comprise metallic pipes and suitable metallic couplings which comply with the relevant requirements of SANS 2001-DP2 or SANS 2001-DP6.

Table 1 — Friction factors associated with a particular diameter of service pipe serving a specified number of fire hydrants and fire hose reels

1	2	3	34	:5	6	7	8	9:	30
Nominal diameter of				Fricti	on factor	for service	e pipes		
pipe		Num		ose reels rvice pip				of fire hydra a service p	
mm	T.	2	-3	4	5	6	1	2	3
25	0,11	0.41	0,86	1,47	2.21	3,11			
32	0,05	61,0	0,38	0,65	0,98	1,38			
40	0,02	0,05	0,10	0,18	0,27	0.37	1	* :	34
50	0.01	0,02	0,04	0.06	0,10	0,13		*	
76	0	0	0	0	0.01	0,02	0,53	1.91	4,05
100	D	0	0	0	0	0	0,11	0,39	0,83
150	- 0	0	0	0	0	0	0,02	0,05	0.11

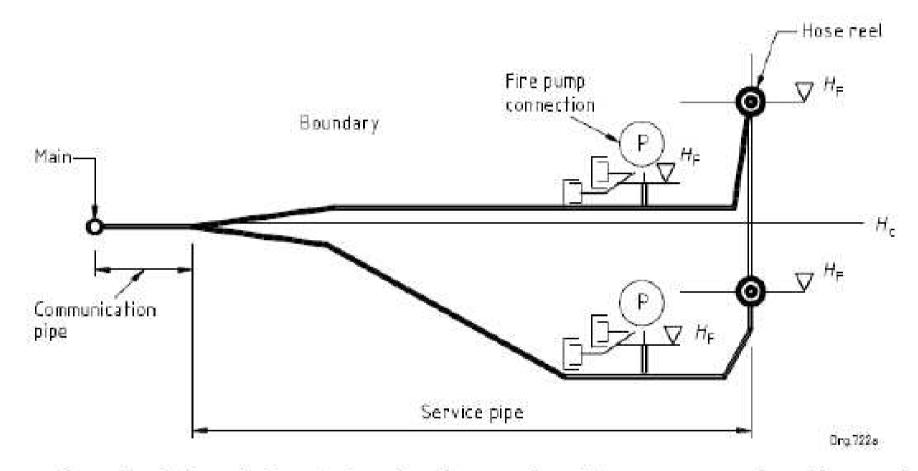


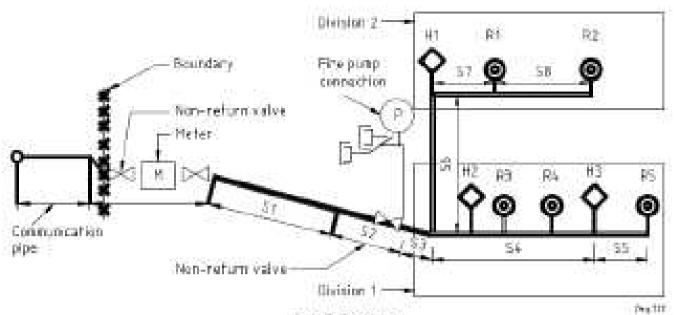
Figure 1 — Schematic layout of service pipes serving a fire pump connection of hose reel

Example of a calculation for sizing pipework

A double-storey building has two fire divisions: one with one fire hydrant and two hose reels, and the other with two fire hydrants and three hose reels.

The static head is measured as being 36 m.

The lengths of service pipes and the elevations of the various hydrants and hose reels are as shown in the figure.



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Hose real	Relative elevation (t)
.81	12
- 62.	32
85	7
(24)	8
96	- 6

Hydrant	Relative elevation m
HBL	127
HD	- 37
113	

Service pipe	Length	Minimum pips dismeter permitted (TIII)
81	-80	75
52	-30	75
53	1	75
84	50	76
55	30	25
55	5.5	76
87	20	26
86	10	25

Connection	Relative elevation m
Fire pump connection	100
Bervice pump - upermentcabor pipe junction	10

Ŷ	may hydrard
9	Flose reel

Service pipe to fire pump connection

The head loss in the service pipe from the communication pipe to the fire pump connection (S1 + S2) for the maximum fire load of the two fire hydrants, is as follows for a 75 mm diameter pipe:

$$PF \ge PM - (HF - HC) - PL$$

= 36 - (5 - 10) - (60 × 1,91 + 30 × 1,91)
= -130,9 m
(< 5 m is unacceptable (see 4.6.1(b)))

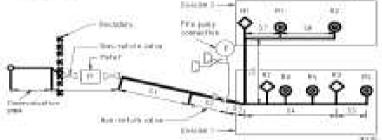
If S1 and S2 are increased to 100mm diameter:

$$PF \ge PM - (HF - HC) - PL$$

= 36 - (5 - 10) - (60 × 0,39 + 30 × 0,39)
= 5,9 m
(> 5 m is acceptable (see 4.6.1(b)))

Table 1 — Pricing factors according with a portunity disperse of service pipe service a specified supplier of the brokests and the base seek.

4.1	94.1	2.81	236	- 81	- 1	1	1.14	0.040	100
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100	- T	330	3.0	34		10.7	1.1	100	1.
	0.11	.0.41	9,46	3.42	18.85	9.31	17.5	3.5	7.5
- 80	0.89	0.10	939	0.66	15,80	139	10.0	- 87	- 6
4	9.68	9.09	1000	5.9	9.00	1037	177	- 1	100
100	100	19.00	3.84	5,00	4.8	0.76	11.75	- * 11	- 1
76		- 8	110	100	0.00	16/00	3.46	1,81	4.85
1980	78	570	356	78.0	7.6	0	1.14	139	7.00
150	- 0	0.1	0.1	1.0	0	.0	1.00	1.01	0.01



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Service pipe from fire pump to hose reels in division 1

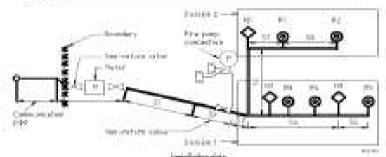
The head loss in service pipes from the communication pipe to hydrant H3 (S1 + S2 + S3 + S4) for three hose reels is 0 as the friction factor for 75 mm and 100 mm diameter service pipes supplying three hose reels is 0 (see table 1).

At R4:
$$PF \ge PM - (HF - HC) - PL$$

= $36 - (6 - 10) - 0$
= 40 m
(> 30 m is acceptable (see $4.6.1(b)$))

Takin 1 ion Printlen Sources assessment with a perfocular diameter of source pipe parving a specified number of the Tryspects and the Inner reals

_	- 8	100	1.6	1	6		10.0	1 3 1	-18
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0.0	4500	8,00	11,040	2036	2000	0,01	10.00	1.0	- 8.5
85.5	0.6	4.1	4.1		30.81	000	0.00	1.00	1.00
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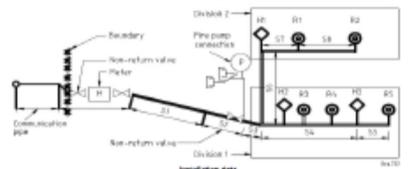
9	ton follows:
9	tank ber

At R5: $PF \ge PM - (HF - HC) - PL$ = 36 - (6 - 10) - 30 × 0,11 = 36,7 m

(> 30 m is acceptable (see 4.6.1(b))) (25 mm diameter pipe is acceptable and there is no need to increase the pipe size)

Table 1 — Priction factors associated with a particular diameter of service pipe serving a specified number of fire hydramic and fire hose resis.

1	2	- 3	4	- 6	- 6	7	- 6	9	10
Nominal diameter of				Prist	on taster	for service	e pipes		
pipe or		Num		coe reelo ervice pig	Derved De			of fire hydro a service p	
EVE	1	2	0	-4			.1	*	
25	0,11	6,01	0,99	1,47	2,21	3,11	- 4	*	
52	0.06	0.18	0.35	0,05	0.96	1,58			
40	9.02	1,08	0.10	9,16	0.27	637	*		
50	0,01	6,02	0,64	0,06	0,10	D(13		*	
75	0	0	0	0	0,01	0.02	0.53	1,91	4.05
100	0	0	0	0	0		0.11	0.39	0.60
150	0	0	0	0	0	. 0	0.02	0.85	0.11



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81	12	141	10
80	12	198	3
86	7	198	- 1
R4	- 4		
65	6		

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Fire pump correction	
Service pump - communication pipe panction	*

Service pipe	Langth	Stanete perioded stanete perioded
781	66	76
107	30	m-
160	- 8	76
.04	90	m
107		27
66	8	79
567	20	27
1586	90	26

Ŷ	Fire hydrant
φ	Plose redi

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Service pipe from fire pump to hose reels in division 2

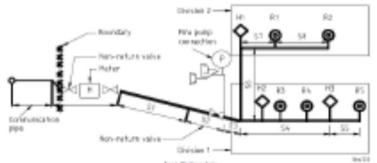
The head loss in service pipes from the communication pipe to hydrant H3 (S1 + S2 + S3 + S6) for two hose reels is 0 as the friction factor for 75 mm and 100 mm diameter service pipes supplying two hose reels is 0 (see table 1).

At R1:
$$PF \ge PM - (HF - HC) - PL$$

= 36 - (12 - 10) - 20 × 0,41
= 25,8 m
(< 30 m is unacceptable (see 4.6.1(b)))

Table 1 — Printion factors associated with a particular diameter of service pipe serving a specified number of fire hadronts and fire hope resis

1	2	3	- 1	5	6	T		19	10
Nominal				Price	on factor	Not senior	e popes		
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mm	1	5	3	4		- 6		2	3
25	0.11	1,41	0.86	1,47	2.21	3,11			*
32	0.05	1.18	638	1,65	0.98	1,36			
40	9.62	1.05	0.10	8,10	9.27	0,87			
50	0.01	1,02	004	8,06	0.10	0.15			
76	0	9	- 1	9	0,81	9,82	0.50	1,91	4.08
100	0	8		- 1	0	ů.	0.11	0,39	0,83
190	0	- tr		- 01	0	0	6.02	0.05	0.11



Here real	Parame Mendion	Hydrani	Parities.
Ge.	192	791	10
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Connection	Name of Street
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pipe parcition pipe parcition	78

Section pipe	Langen	Marimum pipe diameter permitted man
91	- 00	.19
30	30	79
80		79
54	56	75
50	26	12
391		79
807	30	26
444	40	186

Ŷ	PROTYERS
9	Physicsel

Therefore, if S7 is increased to 40 mm diameter:

At R1:
$$PF \ge PM - (HF - HC) - PL$$

= $36 - (12 - 10) - 20 \times 0,05$
= 33 m
(> 30 m is acceptable (see 4.6.1(b)))

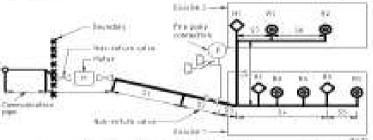
At R2:
$$PF \ge PM - (HF - HC) - PL$$

= $36 - (12 - 10) - (20 \times 0.05 + 10 \times 0.11)$
= 31.9 m

(> 30 m is acceptable (see 4.6.1(b)))
(25 mm diameter pipe is acceptable
and there is no need to increase the pipe size)

Finite 1 — Frighter factors associated with a particular distinctor of very lar pipe serving a specified market of fire bysitiants and fire times rests.

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1.00	0.11	0.41	0.66	6.40	1344	9.31	1.0	100	- 1
10	0.89	0.98	9086	6.66	0,00	138	13.9		11.5
-46	0,01	0.000	0.60	31.50	0.87	18,97	1.5	100	7.0
1.00	0.61	.0000	9064	4,486	0,00	3,78	10.5	- 20	
781	7.8	0.00	1.6	78.	10,01	9,61	3.36	1.81	4.00
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Summary

The pipe sizes in the table are required.

1	2	3		
Service pipe	Length m	Pipe diameter mm		
S1	60	100		
S2	30	100		
S3	5	75		
S4	30	75		
S5 30		25		
S6	5	75		
S7	20	40		
S8	10	25		